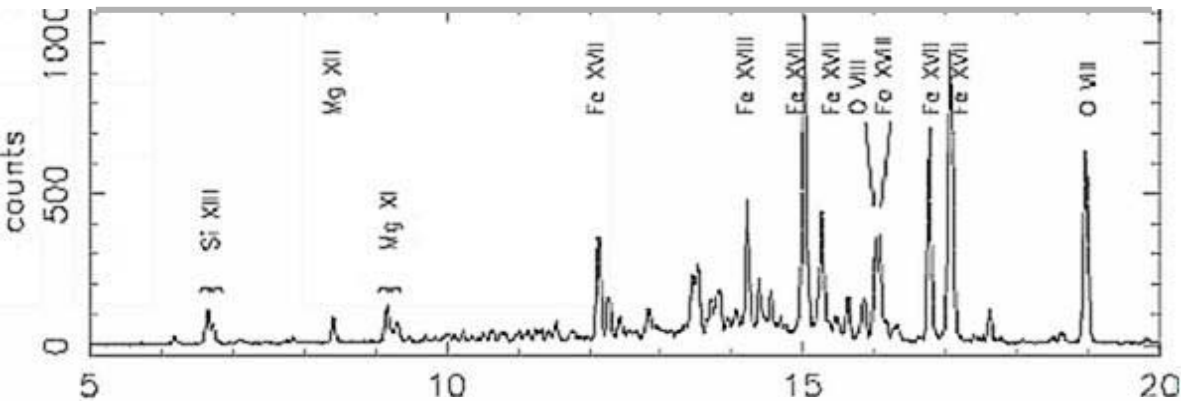


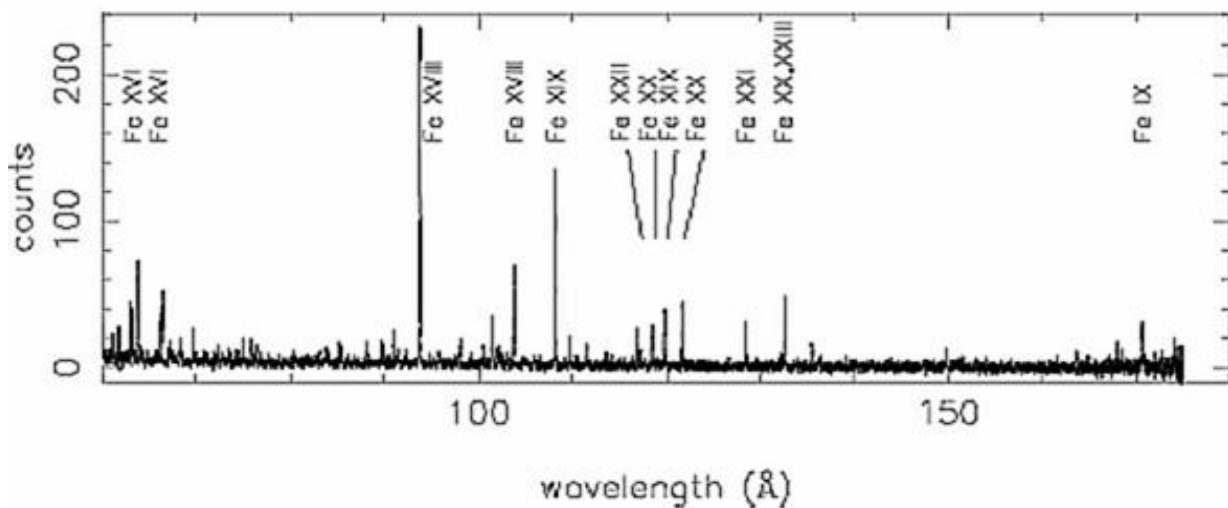
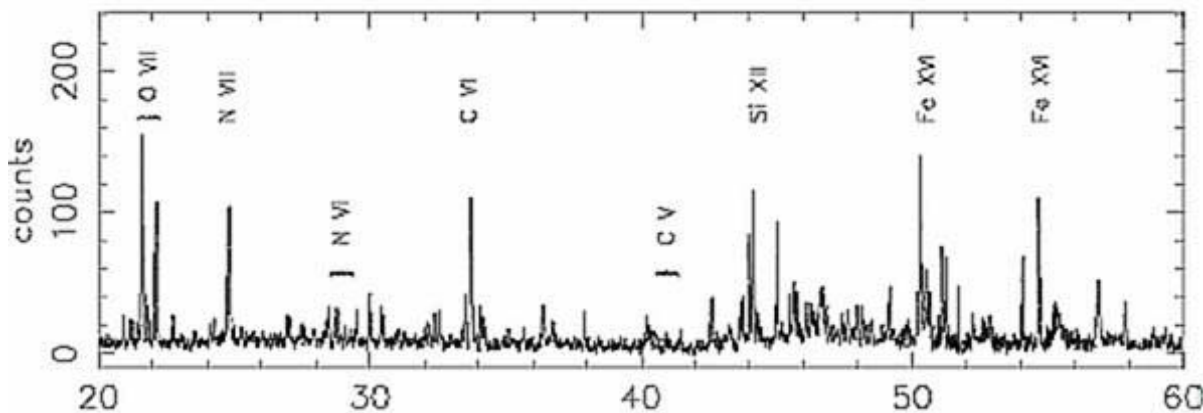
The Off-Plane Option for the Reflection Grating Spectrometer

Webster Cash

University of Colorado



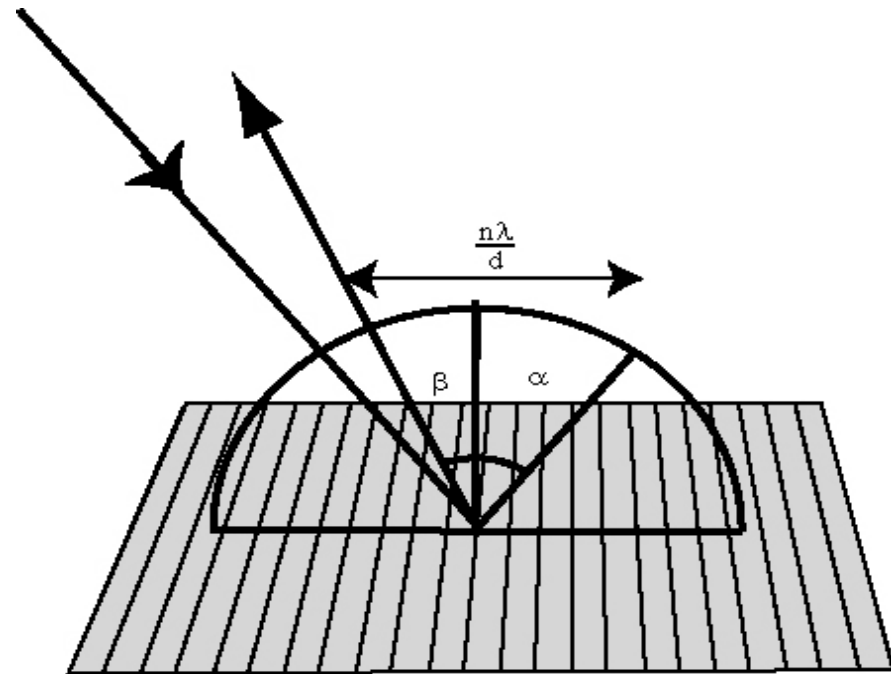
Chandra Spectra Look Like Traditional Ground Spectra.



Can We Afford to Step Back???

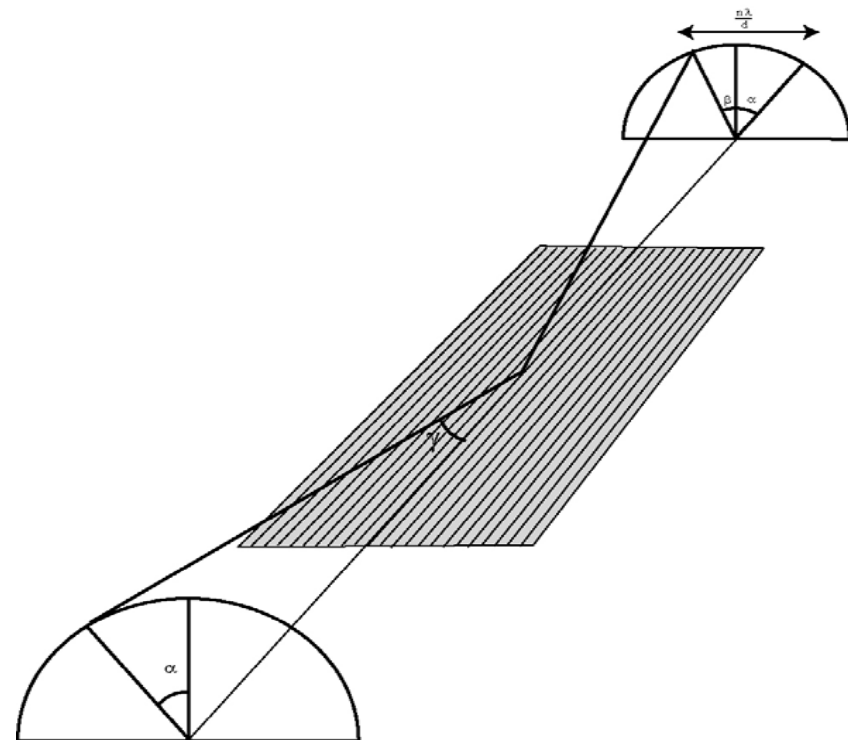
In-plane Mount

$$\sin \alpha + \sin \beta = \frac{n\lambda}{d}$$

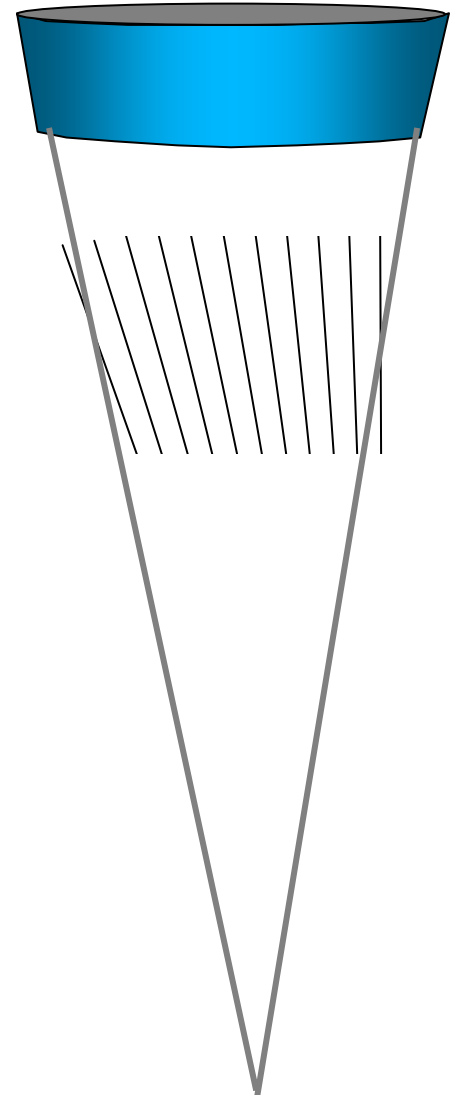
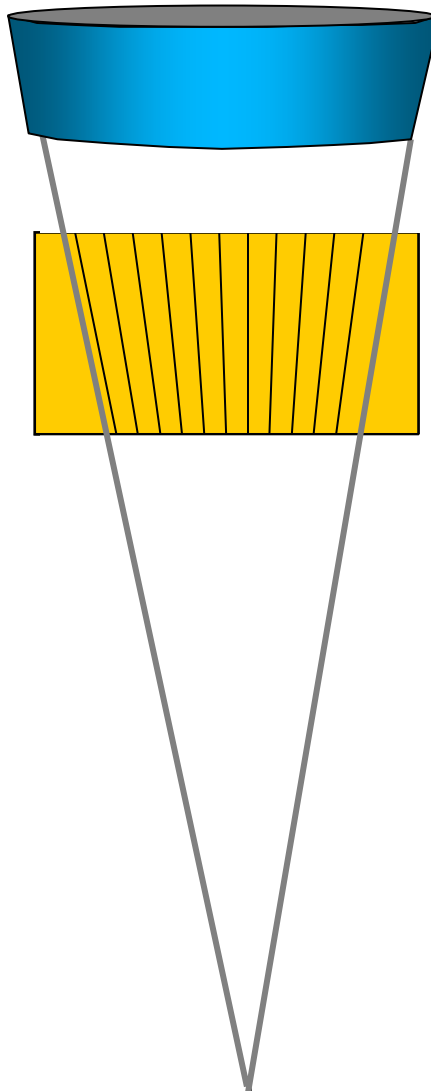
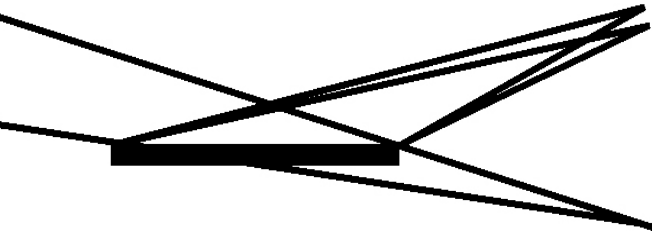
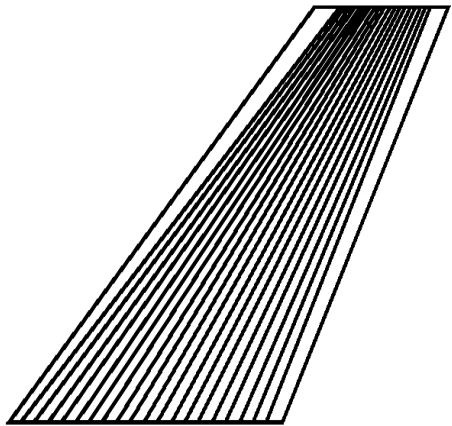


Off-plane Mount

$$\sin \alpha + \sin \beta = \frac{n\lambda}{d \sin \gamma}$$



Radial Groove Gratings



Off-plane Resolution

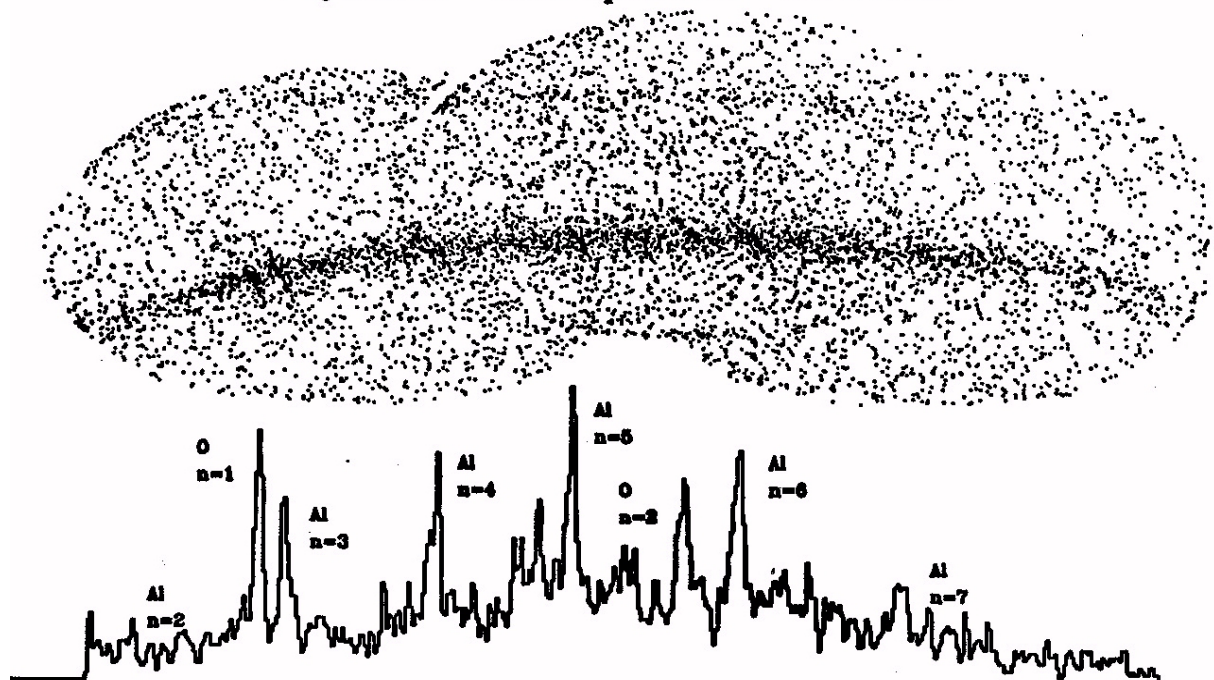
$$R = \frac{(\sin \alpha + \sin \beta) \sin \gamma}{B \cos \alpha}$$

At typical values of off-plane angles and 15'' telescope resolution
R ~ several hundred → thousand

Sub-Aperturing improves it further

An Off-plane X-ray Spectrum

Al Spectrum - XOGS Spectrum - MSFC Beam



Spectrum from Al target shows Al $K\alpha$ ($\lambda=8.3\text{\AA}$, $E=1.4\text{keV}$) in orders $n=2$ through $n=7$. Contamination from O $K\alpha$ ($\lambda=23.8\text{\AA}$, $E=0.525\text{keV}$) is also clearly present in first and second orders. Note that the blaze function is about 20 deg. in azimuthal angle. This spectrum was obtained by the XOGS spectrograph in the beam facility at Marshall Space Flight Center using a 3600 g/mm grating array in the off-plane mount. The signal in the sum of orders 3 through 6 is about 40% of the incident signal. With a CCD these orders can be recombined without loss of signal or resolution.

Off-plane Tradeoffs

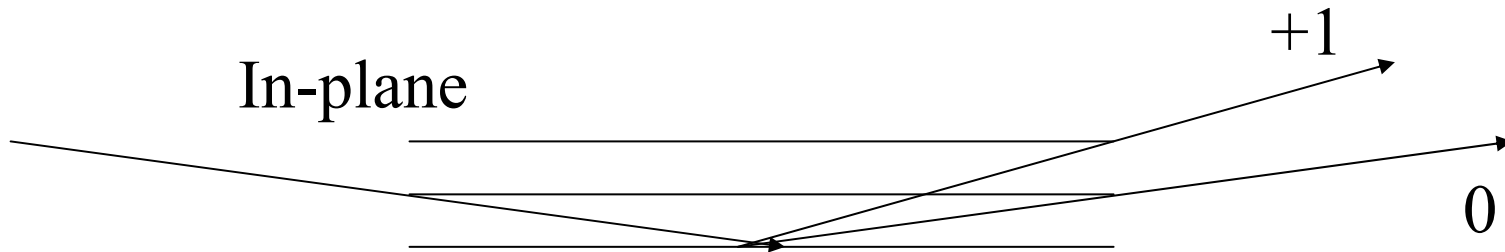
PRO

- Higher Throughput
- Higher Resolution
- Better Packing Geometry
- Looser Alignment Tolerances

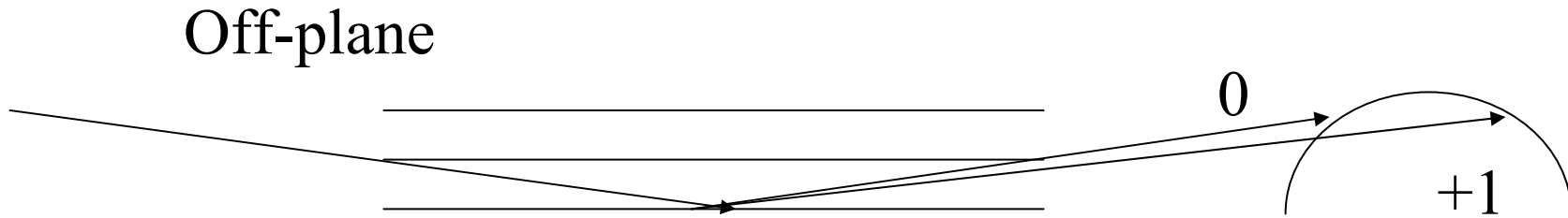
CON

- Higher Groove Density

Packing Geometry



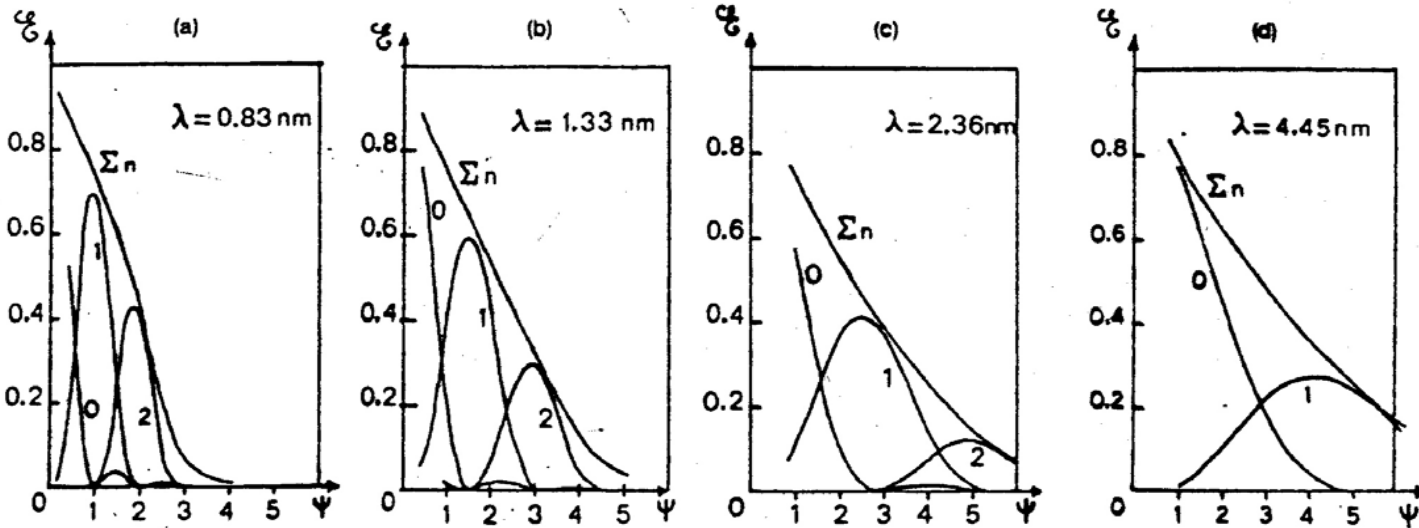
Central grating must be removed.
Half the light goes through.



Gratings may be packed optimally

Throughput

- Littrow configuration $\alpha = \beta =$ blaze angle
 - Better Groove Illumination
 - Maximum efficiency
- Constant Graze Angle



Holographic Gratings

Last year we reviewed approaches to fabricating high density gratings.

At Jobin-Yvon (outside Paris)

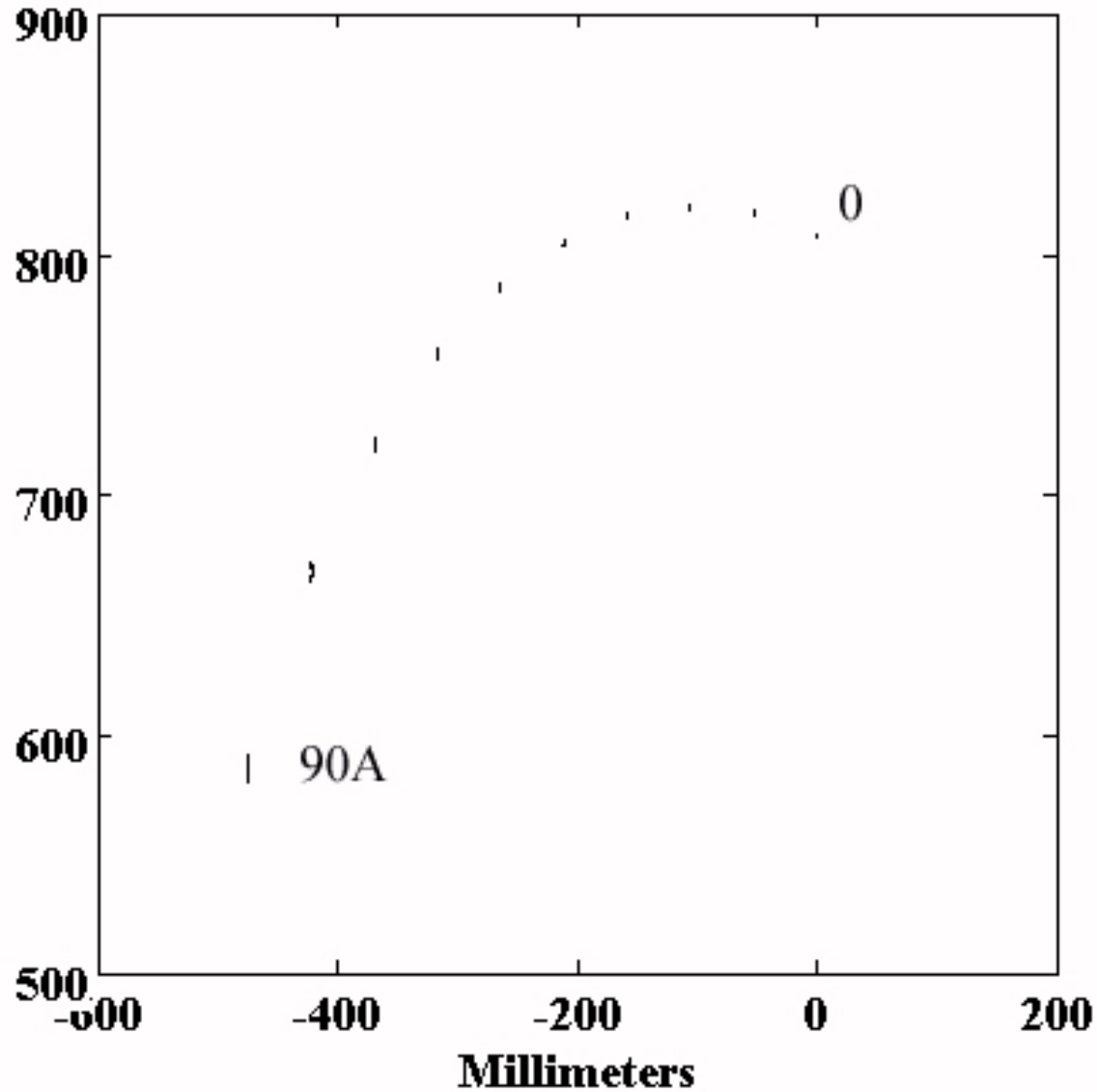
Create rulings using interference pattern in resist
Ion-Etch Master to Create Blaze

Radial Geometry – Type 4 Aberrated Beams

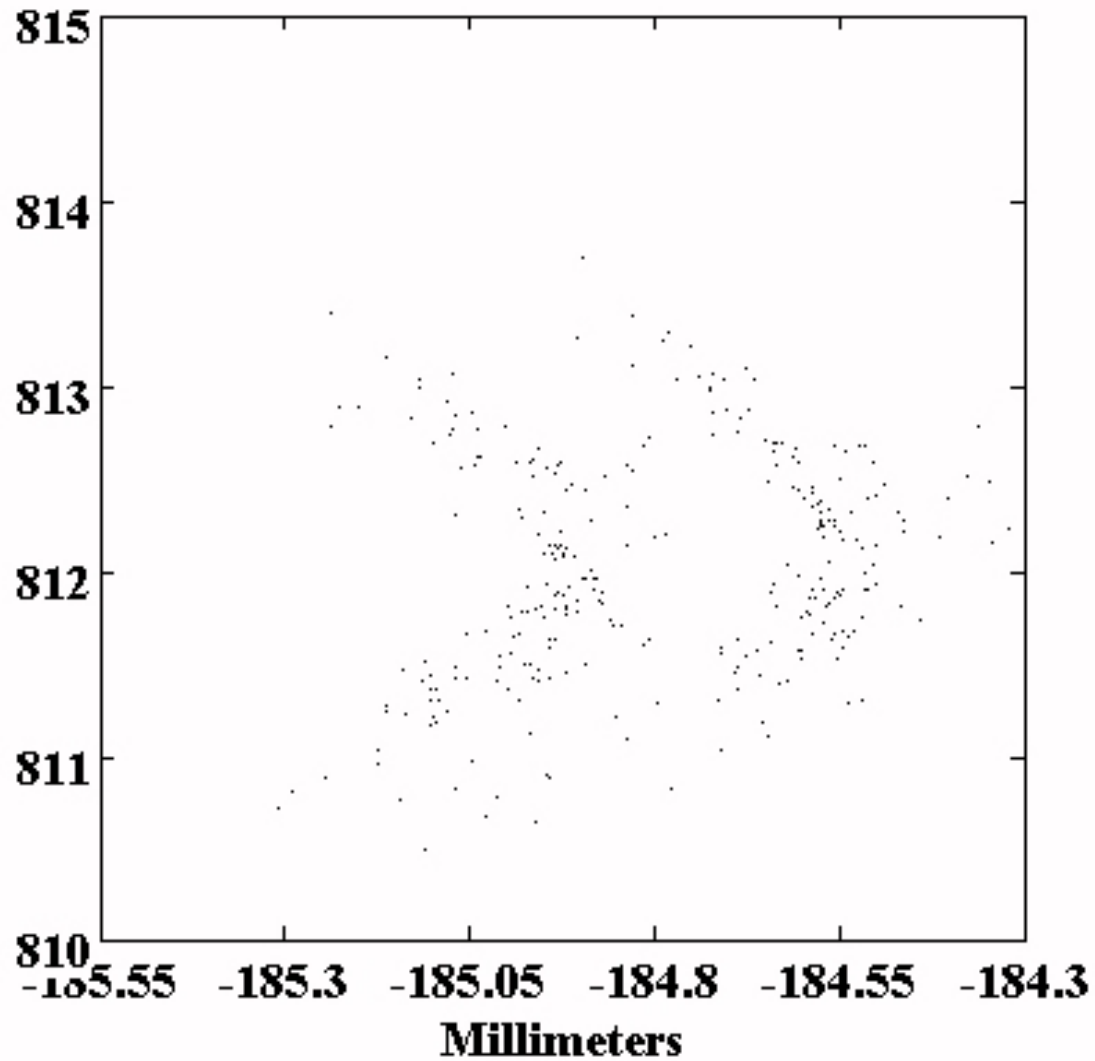
Density: Up to 5800 g/mm Triangular (<35 deg blaze)

In UV holographic blazed gratings have *very* low scatter and good efficiency – same in x-ray?

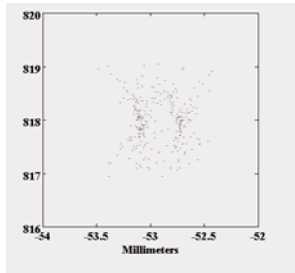
Raytracing – Arc of Diffraction



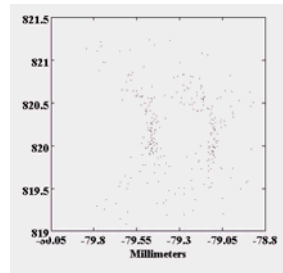
Raytrace – 35 & 35.07Å



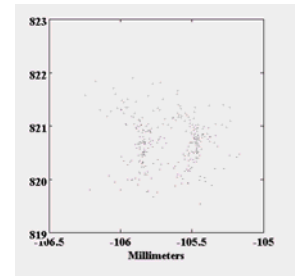
Raytracing of Wavelength Pairs λ and $\lambda + .07\text{\AA}$



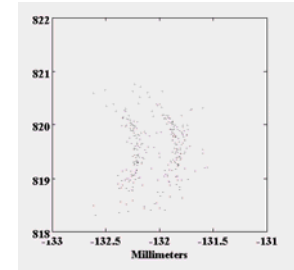
10Å



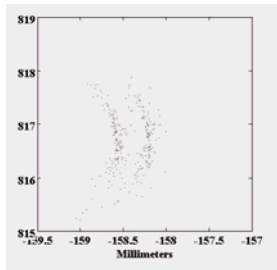
15Å



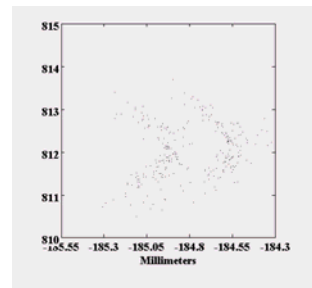
20Å



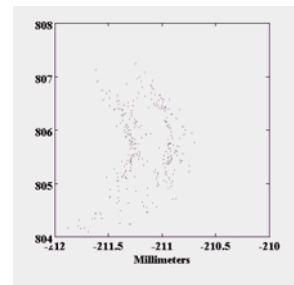
25Å



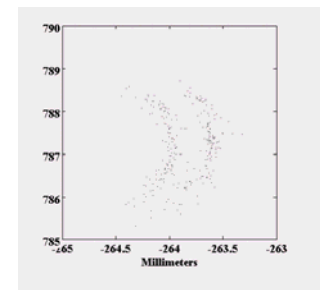
30Å



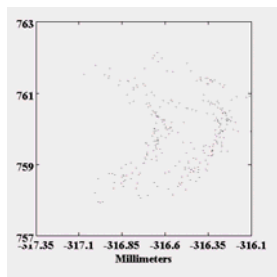
35Å



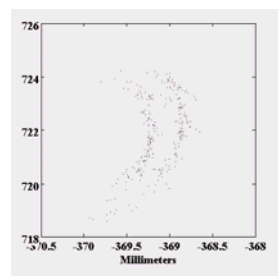
40Å



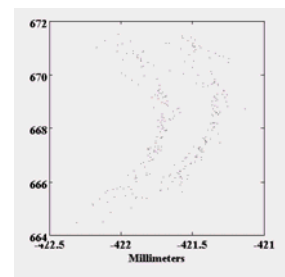
50Å



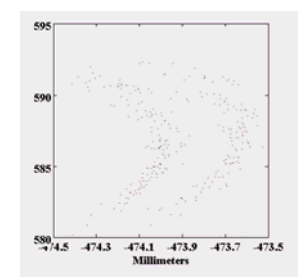
60Å



70Å



80Å

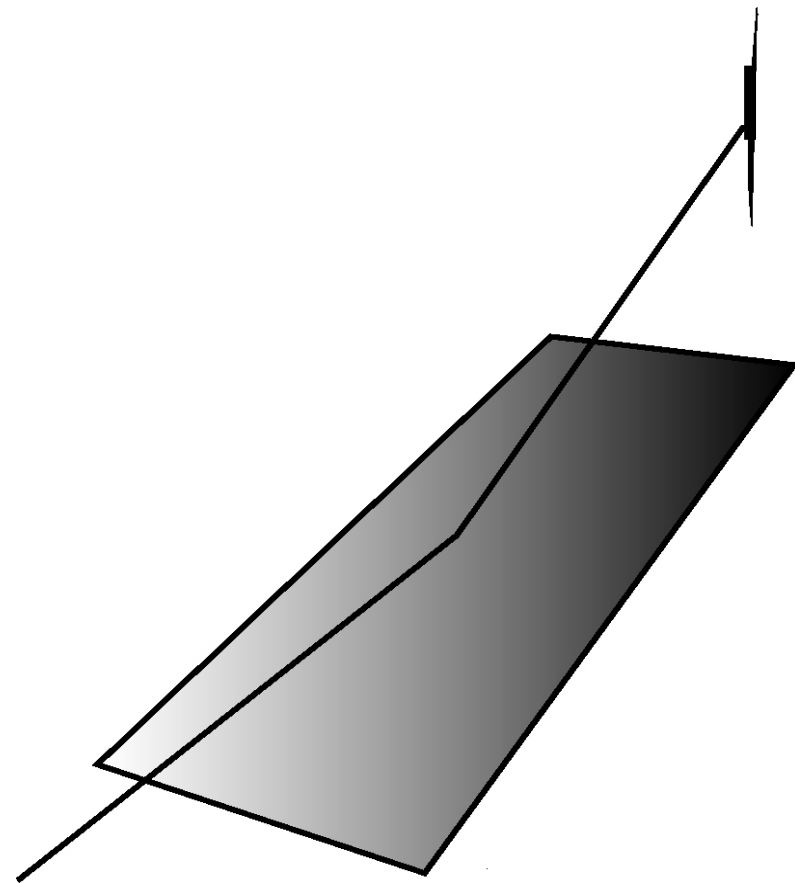


90Å

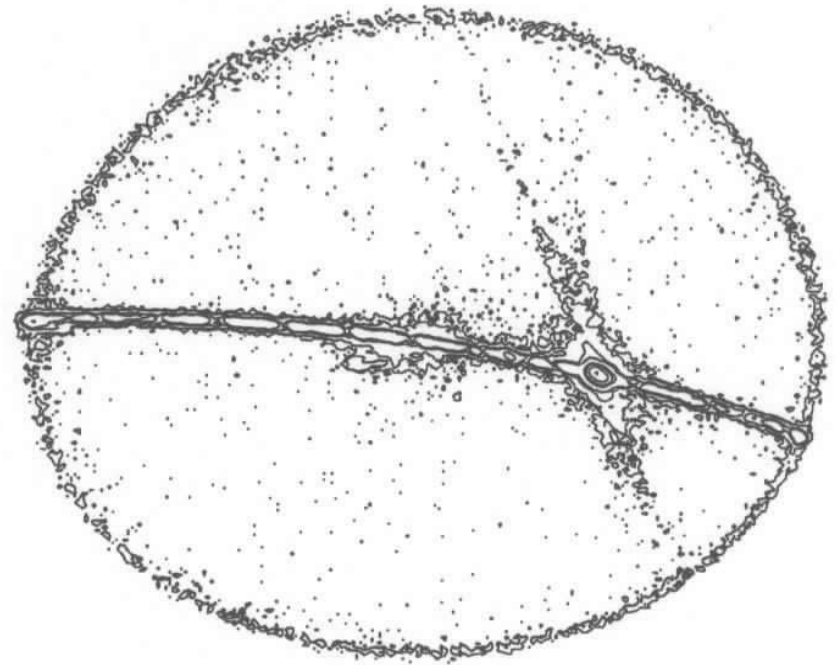
Internal Structure of Telescope

Curvature Favors Dispersion in Off-plane Direction

In-Plane Scatter

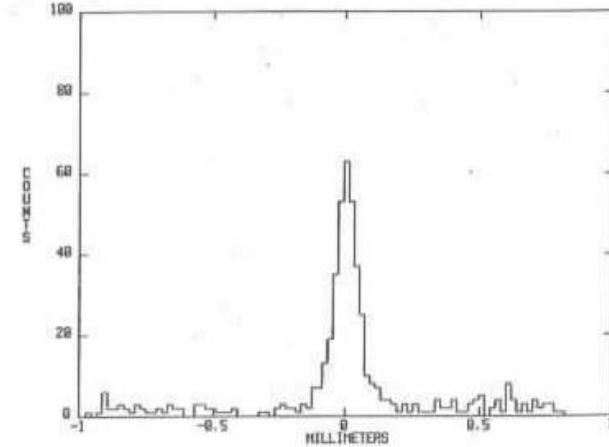
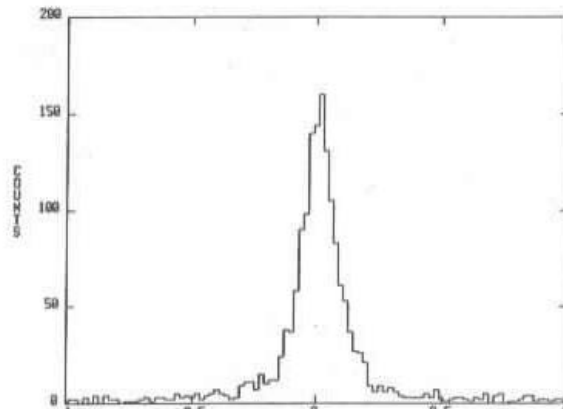
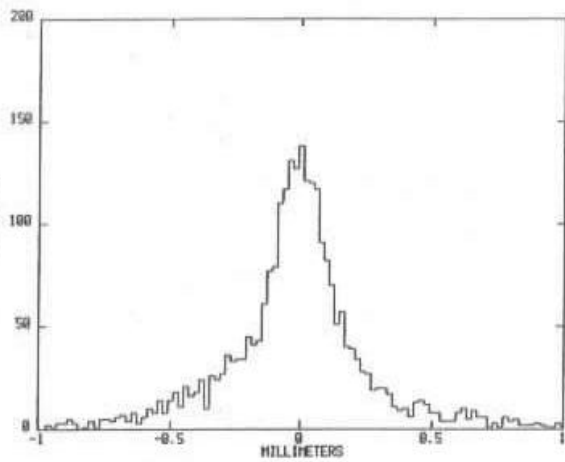
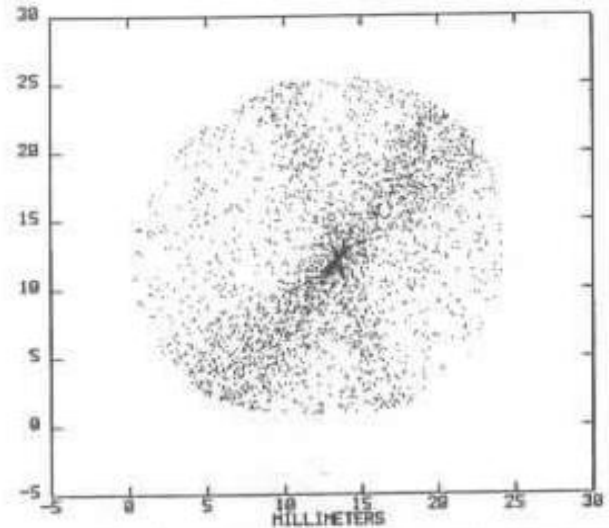
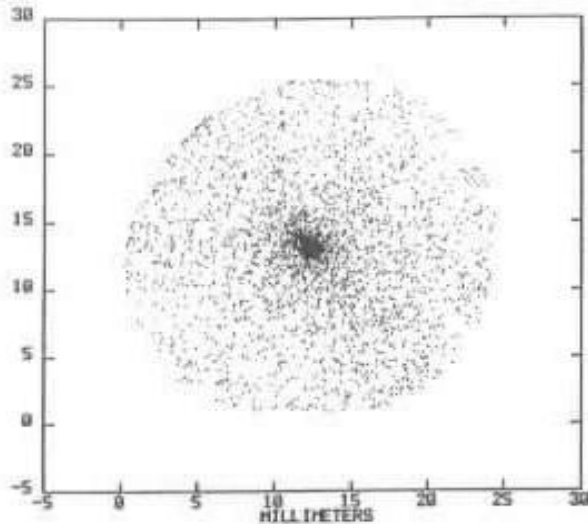


Spectral line of HeII 304Å
displaying In-plane scatter

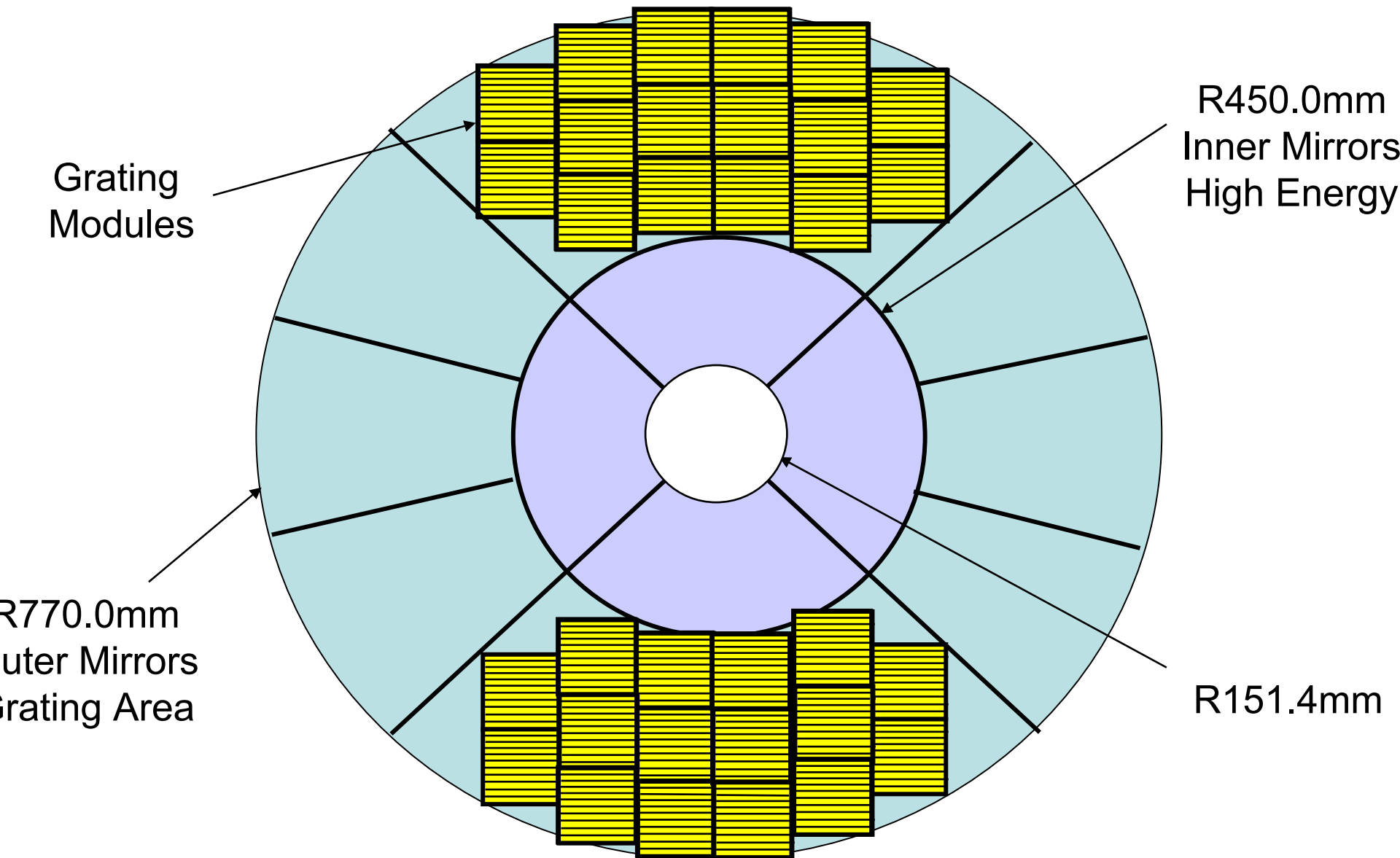


Data from a radial grating in the
off-plane mount, Wilkinson

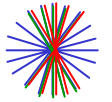
Subaperture Effect



Off-plane Grating Module Locations on Envelope



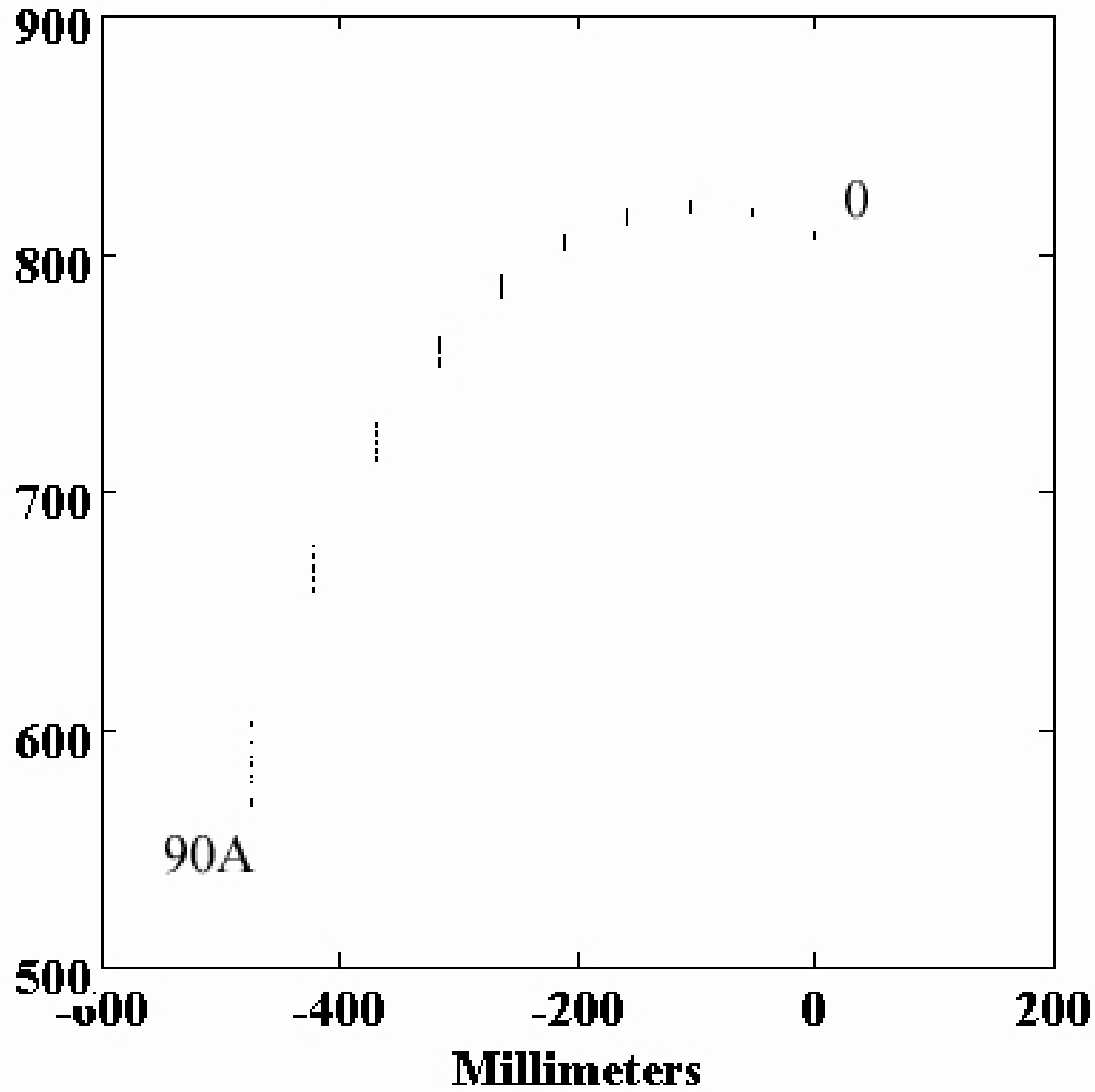
Can Improve Performance



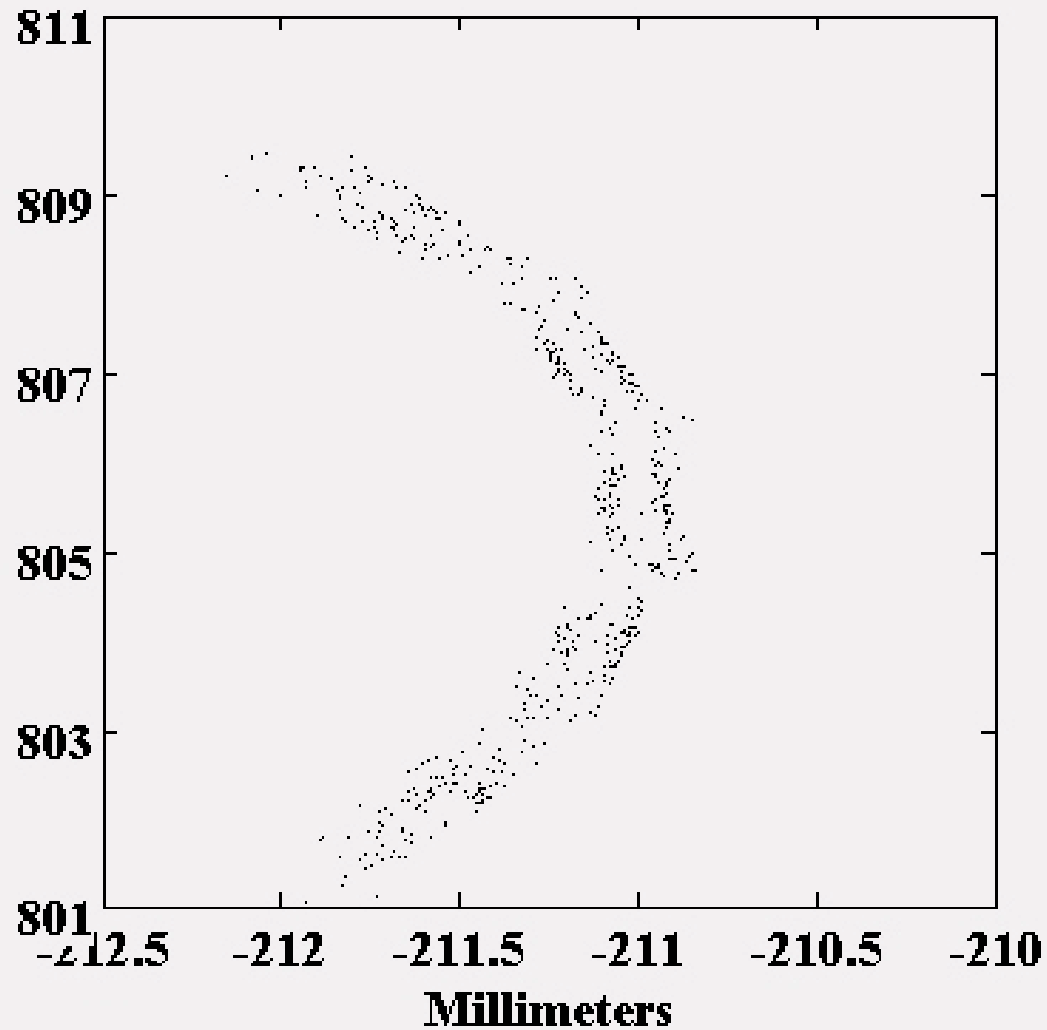
Can Improve Performance



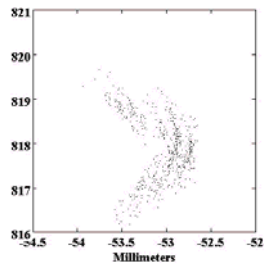
Raytracing – Arc of Diffraction



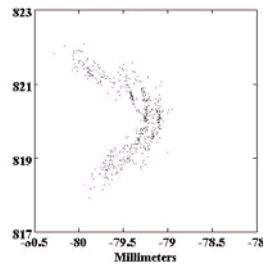
Raytrace – 35 & 35.028Å



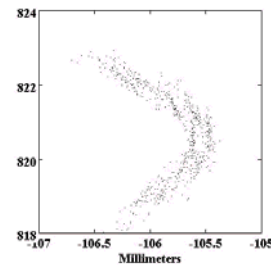
Raytracing of Wavelength Pairs λ and $\lambda + .028\text{\AA}$



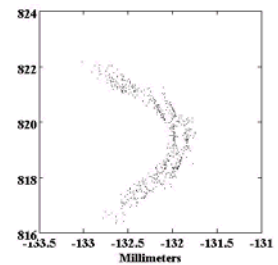
10Å



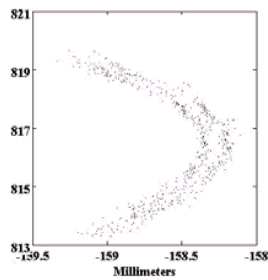
15Å



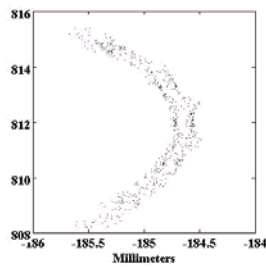
20Å



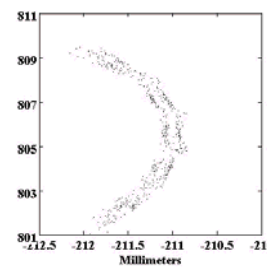
25Å



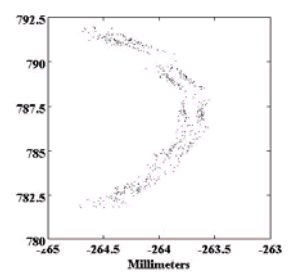
30Å



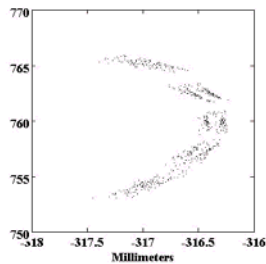
35Å



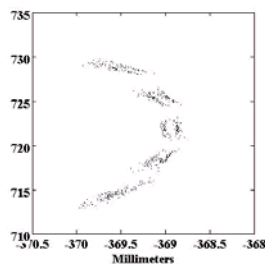
40Å



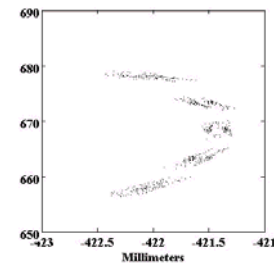
50Å



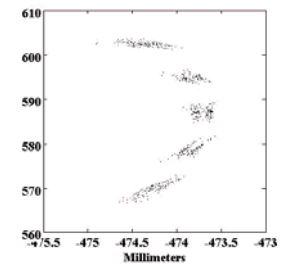
60Å



70Å

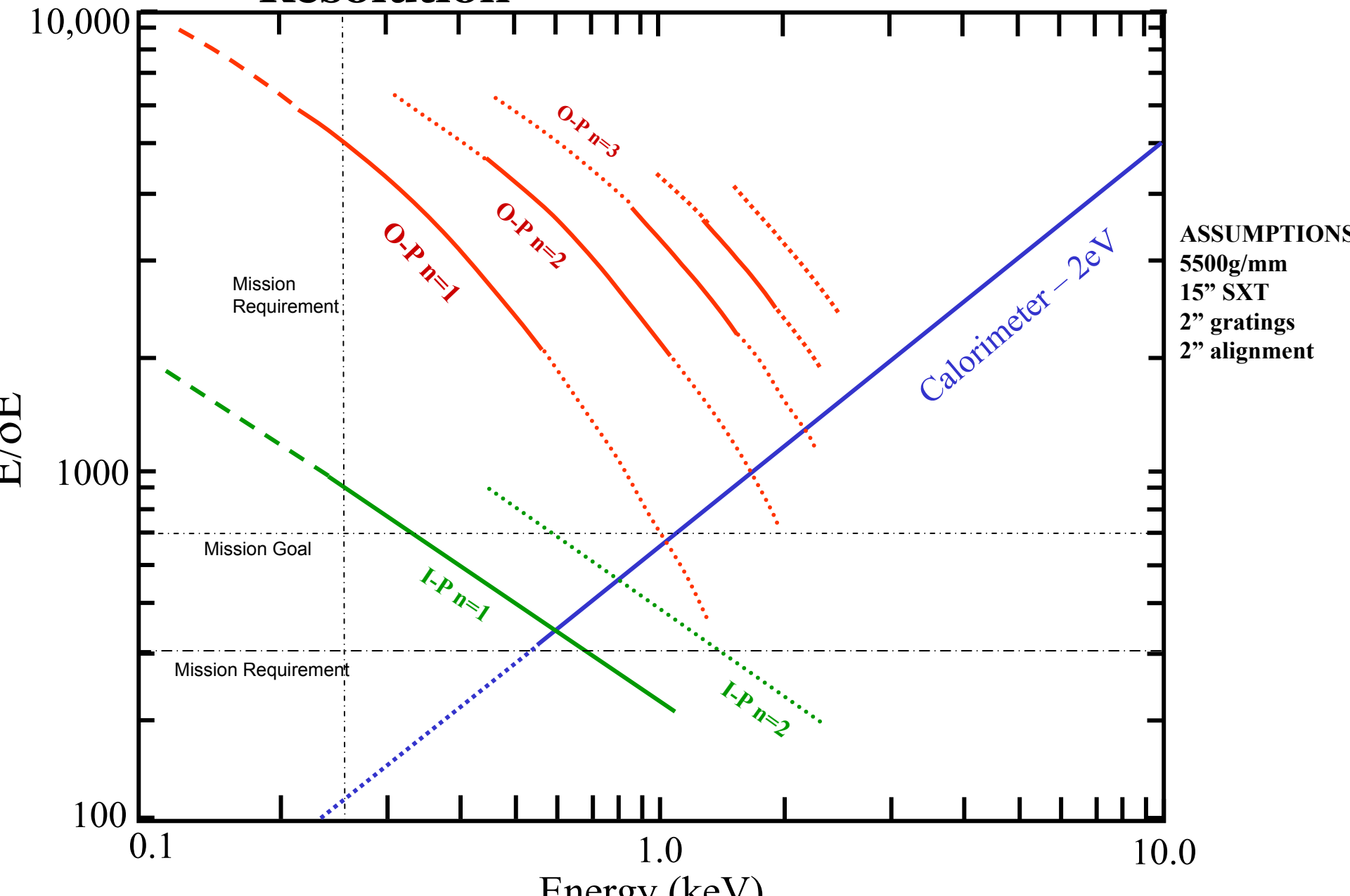


80Å

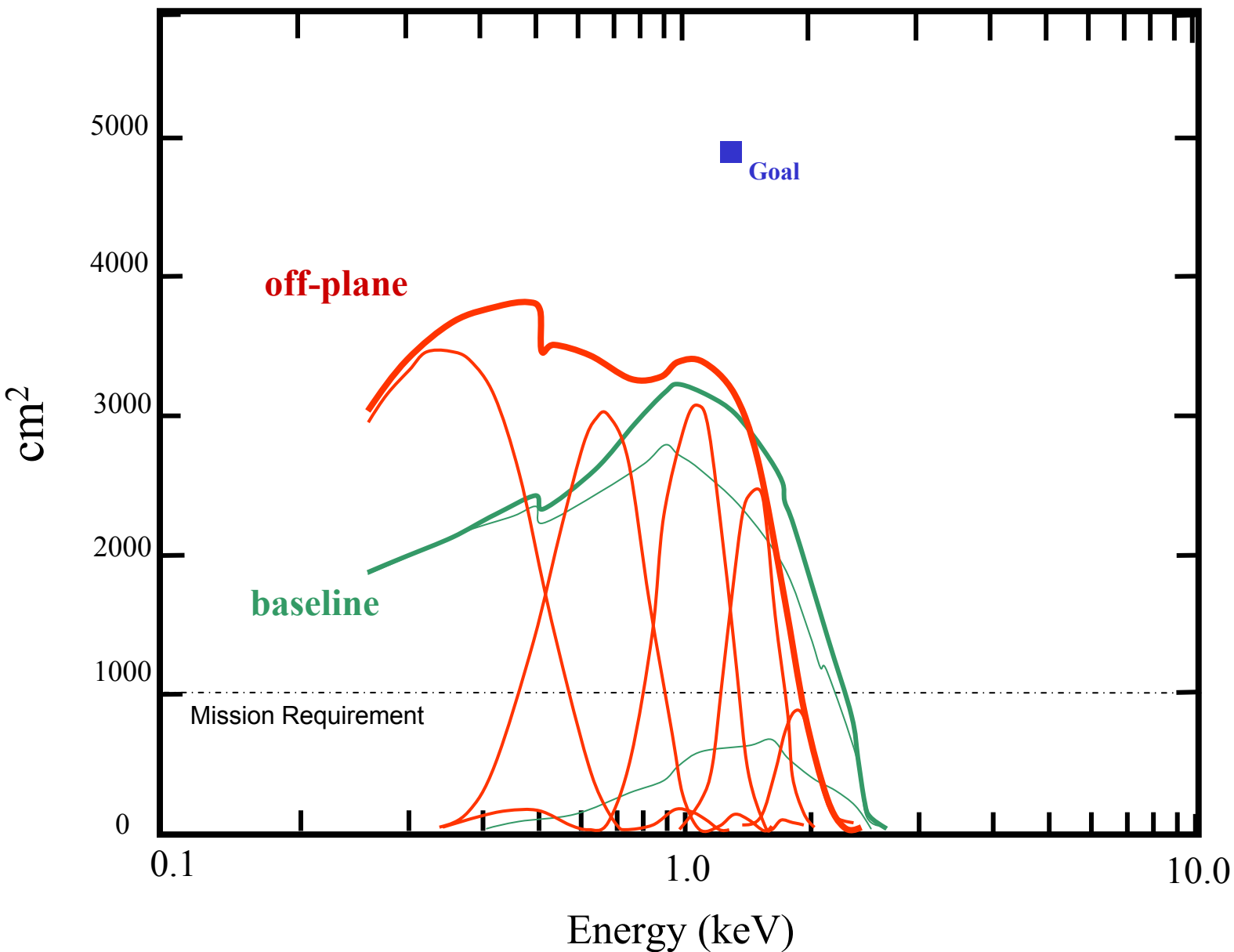


90Å

Resolution



Effective Area



ASSUMPTIONS:
Coverage 40% of
outer envelope
Off-Plane Groove
Efficiency 80%
of theoretical
85% Structure
Transmission
CCD thin Al filter
only

Figure of Merit

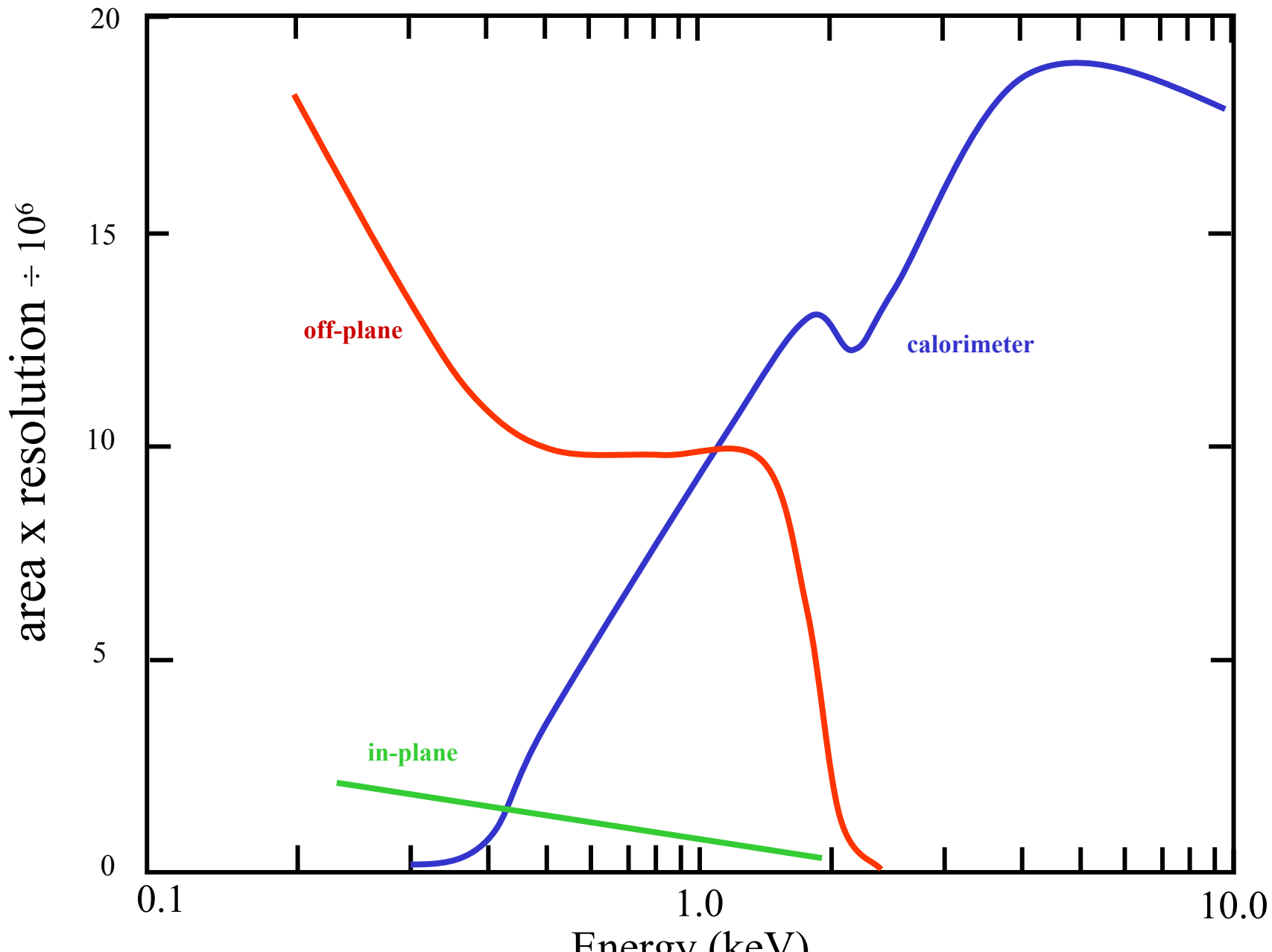
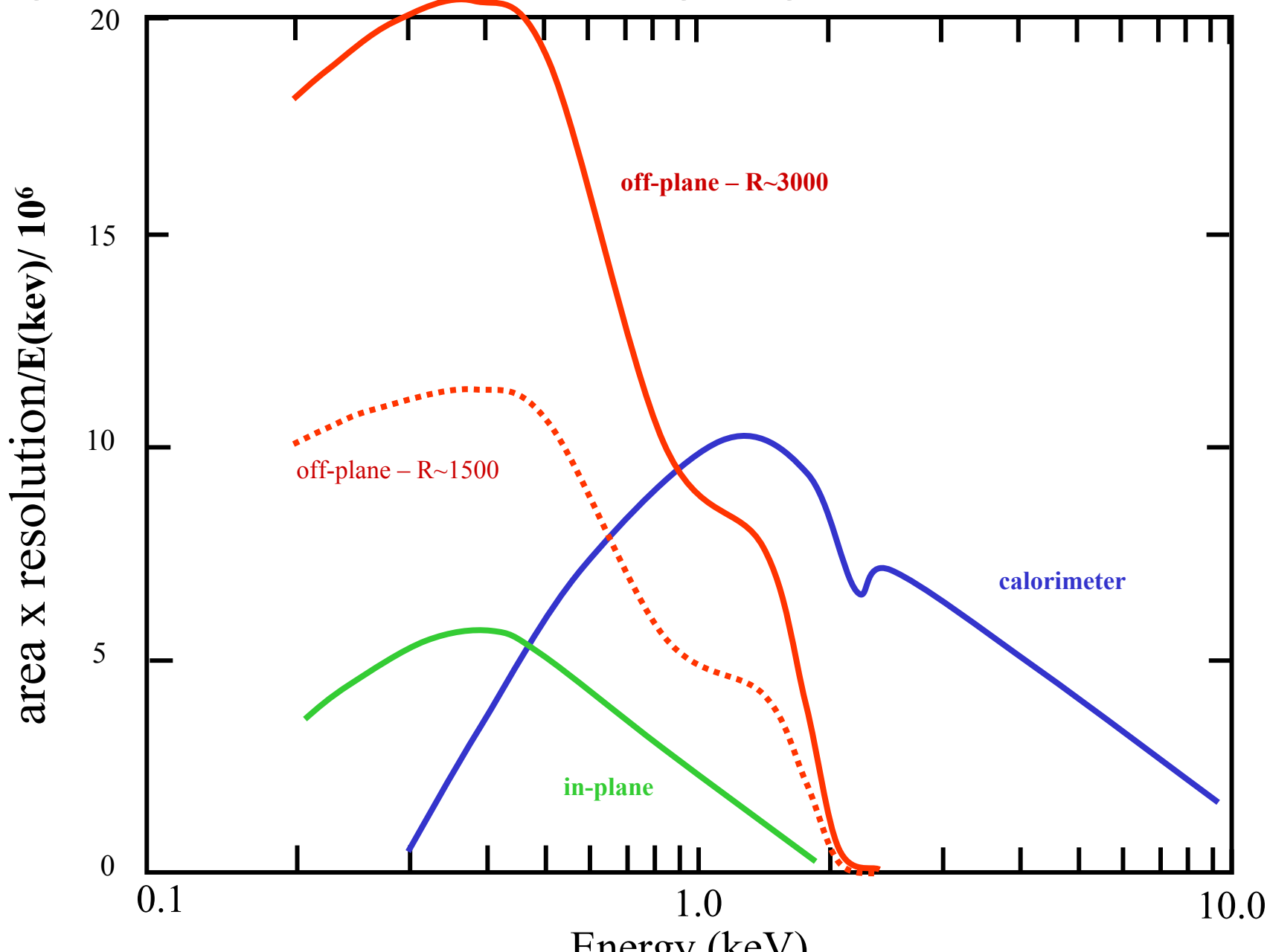


Figure of Merit with Spectral Weighting



Pros & Cons of Off-plane vs. Baseline Design

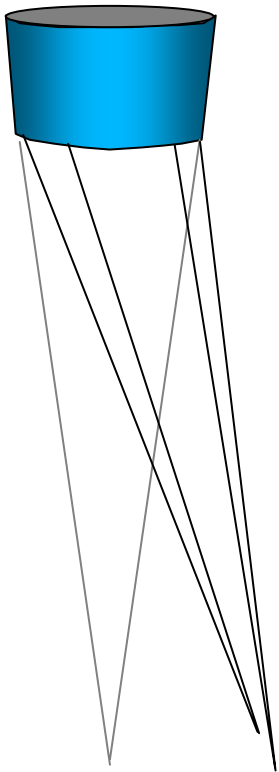
- Pro:
 - Greater Resolution from Sub-aperturing
 - Greater Collecting Area – higher groove efficiency
 - Less Sensitivity to Grating Alignment
 - Less Sensitivity to Grating Flatness
 - Lower scatter in Dispersion Direction
 - Fewer Gratings Required
 - Thicker Substrates Acceptable
 - Smaller Structure Required
- Con:
 - Higher groove density required

Difficulties of High Resolution ($\lambda/\Delta\lambda > 1200$)

- flatter gratings
- tighter alignment
- tighter focus
- telescope depth of focus adjustment
- zero order monitor essential to aspect solution
- more difficult calibration
- greater astigmatism
 - higher background
 - more source overlap

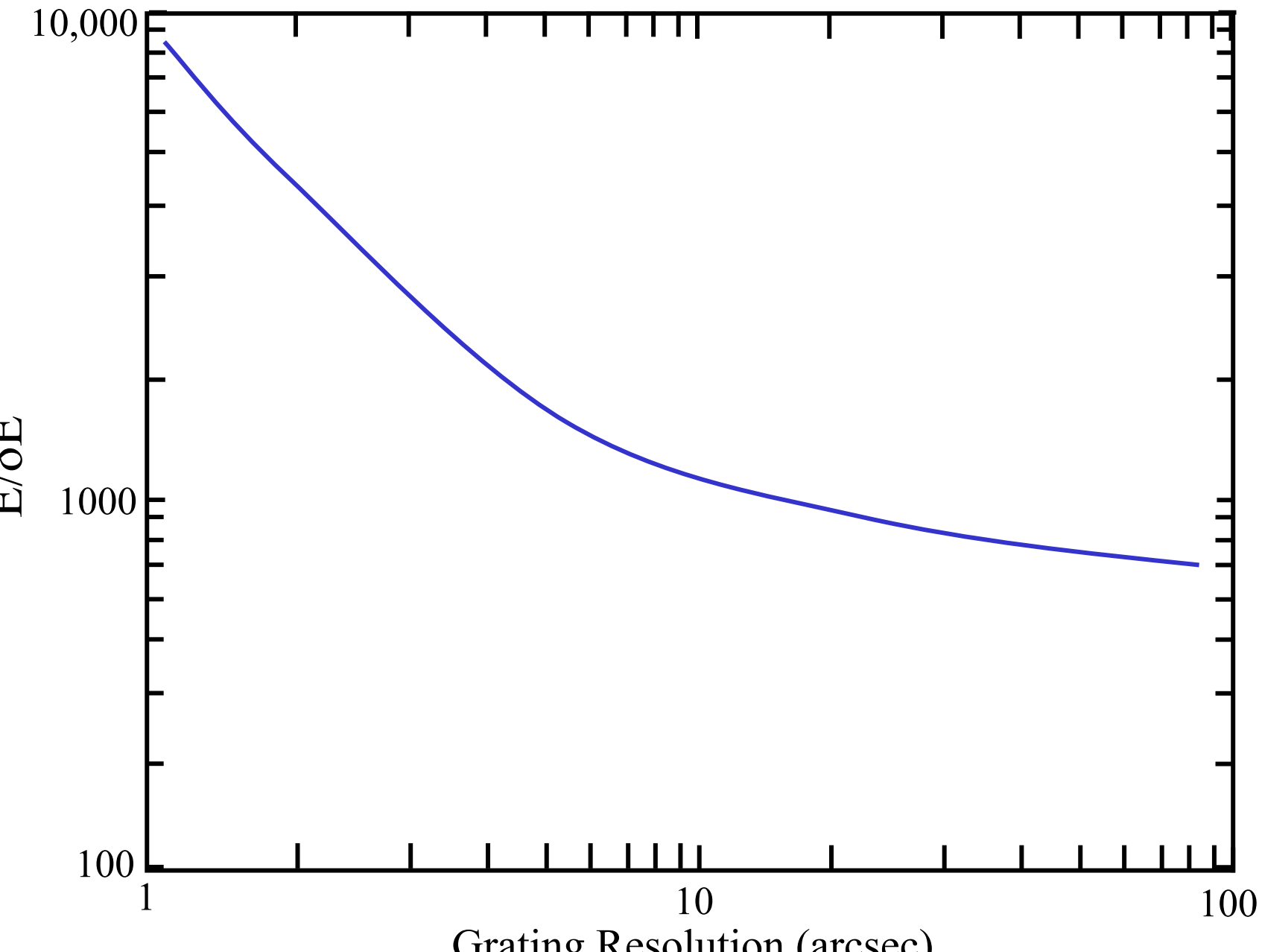
Depth of Field Problem

Solutions for Study:
Smaller Gratings
Curved Gratings
Adjust Telescope Segments

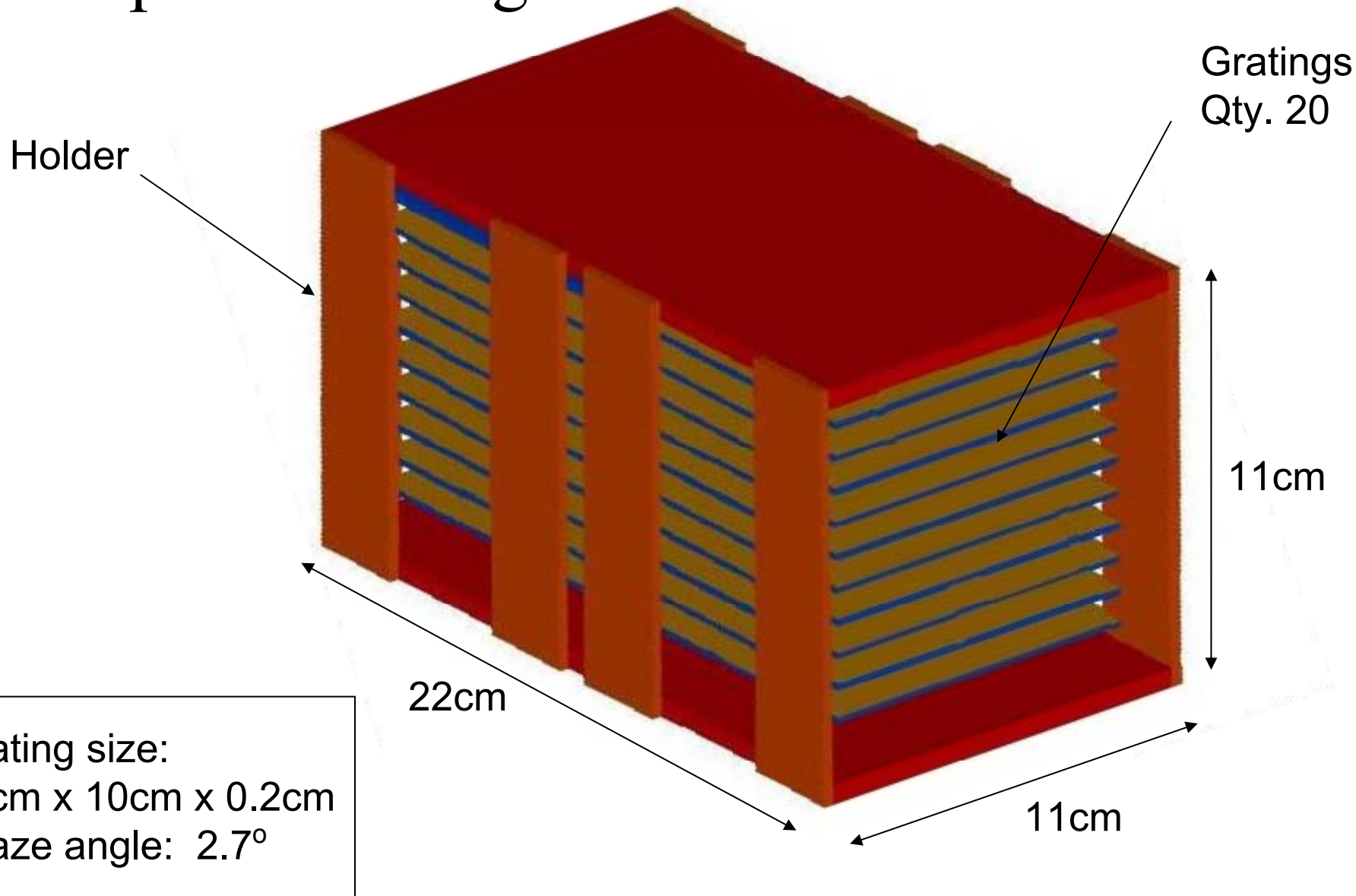


*Hope that it is
merely a matter of
mounting existing shells
at different radii*

Resolution Degradation



Off-plane Grating Module



Off-plane Grating Resolution Options

$\lambda/\delta\lambda \sim 1000$

- SXA (Al/SiC) substrates
- Easy tolerances
- Simple mount
- No thermal gradient
- Mass OK

$\lambda/\delta\lambda \sim 5000$

- Glass/Si substrates?
- More difficult tolerances
- More difficult mount
- Probable thermal gradient issues
- Mass constraint more difficult to meet

Off-plane Grating Estimated Tolerances

Error type	Zero-order Allowable Tolerances		
	Equation	$\omega = 15$ arcsec	$\omega = 2$ arcsec
<i>Surface error</i>	$\delta = \frac{s}{20}$	36.5 μm	4.9 μm
δ_x	$\delta_x = \frac{s}{20 \cos \theta}$	36.5 μm	4.9 μm
δ_y	$\delta_y = \frac{w}{10}$	1mm	1mm
δ_z	$\delta_z = \frac{s}{20 \sin \theta}$	775 μm	103 μm
θ_x	$\sin \phi = \frac{w}{5h}$	11.5°	11.5°
θ_y	$\phi = \frac{\omega}{20}$	0.75 arcsec	0.1 arcsec
θ_z	$\phi = \frac{\omega}{10 \sin \theta}$	31.8 arcsec	4.2 arcsec

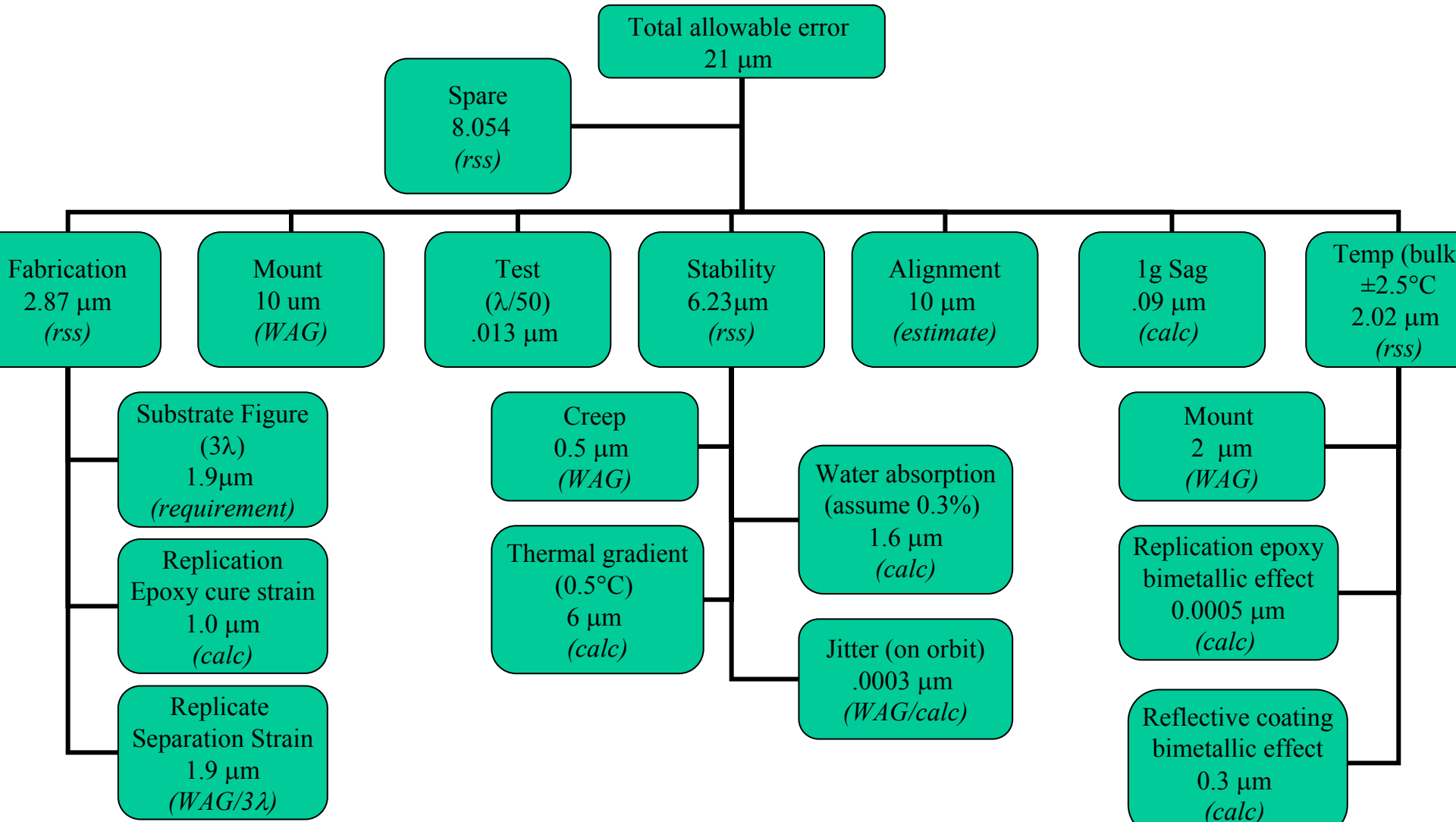
Off-plane Grating Module

Estimated Mass

Materials	Gratings (Kg)	Holder (Kg)	Light- weight	One Module (Kg)	Qty Modules	Total mass (Kg)
SXA/SXA	1.16	1.20	none	2.36	32	75.65
SXA/SXA	1.16	1.20	25%	2.17	32	69.53
SXA/6061	1.16	1.11	none	2.27	32	72.73
FS/Invar/Ti	0.88	1.568	70%	2.45	32	78.36
FS/Titanium	0.88	1.488	30%	2.37	32	75.82
FS/GrEp/Invar	0.88	1.687	none	2.57	32	82.17

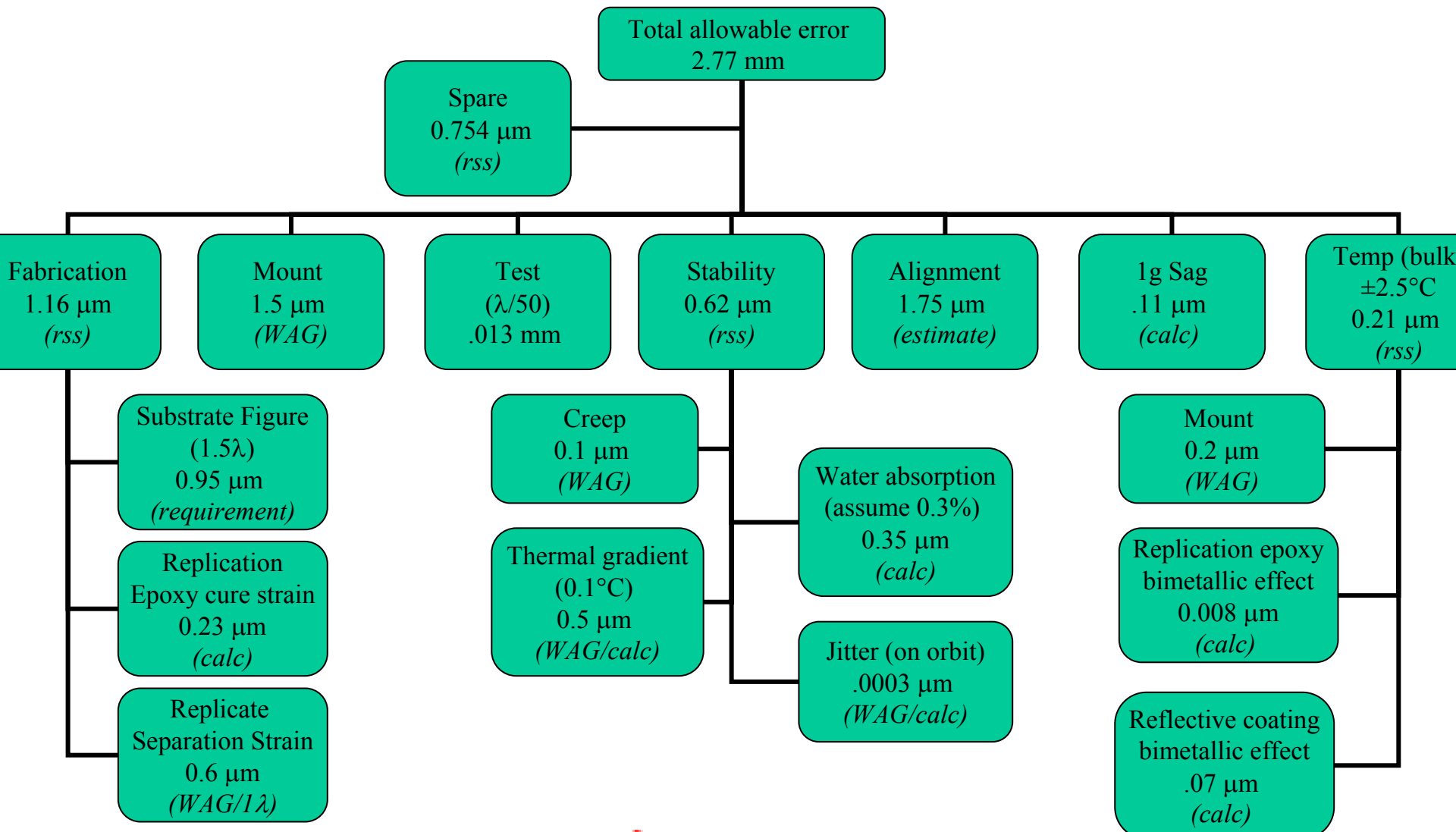
Wavefront Error: Resolution 1000

Constellation X Off-plane Grating Mount rms Wavefront Error Budget (15 arcsec max)
All errors are presented as rms wavefront error



Wavefront Error: Resolution 5000

Constellation X Off-plane Grating Mount rms Wavefront Error Budget (2 arcsec max)
All errors are presented as rms wavefront error



Off-plane Grating Prototype: steps and schedule

Phase	Task	Leadtime
1	Preliminary feasibility study of type 4 aberration corrected grating distribution to approximate radial distribution	4-5 mos. (Jun '02 to ~Oct '02)
2	Preliminary study of blaze process using existing masks (30° profile goal). (work done in parallel with step 1)	4-5 mos. (Jun '02 to ~Oct '02)
3	Contingent upon step 1&2 positive result. Deliverable: 58x58x10mm parallel groove sample with 30° blaze angle.	4 mos. (Oct '02 to ~Feb '03)
4	Contingent upon positive test of sample. Deliverable: 58x58x10mm radial groove distribution with blazed profile.	3 mos. (Mar '03 to ~Jun '03)
5	Ray-tracing to optimize recording configuration Deliverable: 120mm square radial distribution with blazed profile and flight groove density.	TBD

In Conclusion, Off-plane Can:

- Match RGS to Calorimeter Scientifically
 - R~1500
 - greatly eased tolerances
- or Significantly Enhance Con-X Science
 - R~3000
 - tolerances at currently expected levels

Study funded by the Con-X project. First results in January.